This application note explains the content of Nexperia Power GaN FET data sheets. Nomenclature, pinning and key parameters are detailed.
1. Introduction

This application note examines in detail the data sheet for the GAN063-650WSA GaN FET device from Nexperia. Visit the product information page on Nexperia.com to download the latest version of the full data sheet.

2. Nomenclature

The device name (type number) is shown at the top of the data sheet. The name contains some important information about the device. In the below example for GAN063-650WSA, the maximum on-state resistance and the limiting drain-source voltage are specified, together with letter codes indicating the package, the mounting base electrical connection and the technology generation.

![GaN FET Nomenclature Diagram]

**Fig. 1. GaN FET Nomenclature**

W = package code TO247
S = TAB connected to Source
A = Nexperia technology generation 1

3. Pinning information

<table>
<thead>
<tr>
<th>Pin</th>
<th>Symbol</th>
<th>Description</th>
<th>Simplified outline</th>
<th>Graphic symbol</th>
</tr>
</thead>
<tbody>
<tr>
<td>1</td>
<td>G</td>
<td>gate</td>
<td>mb</td>
<td></td>
</tr>
<tr>
<td>2</td>
<td>S</td>
<td>source</td>
<td></td>
<td></td>
</tr>
<tr>
<td>3</td>
<td>D</td>
<td>drain</td>
<td></td>
<td></td>
</tr>
<tr>
<td>mb</td>
<td>S</td>
<td>mounting base; connected to source</td>
<td></td>
<td></td>
</tr>
</tbody>
</table>

The Nexperia GAN063-650WSA is packaged in a TO247 (SOT429) package with a source tab. The traditional TO-247 provides excellent heat transfer, and therefore excellent power-handling capability.
Note: the pin functions are different from a standard MOSFET: pin 1 is the gate, pin 2 is the source and pin 3 is the drain.

Using pin 2 as the source pin allows the circuit designer to keep the gate loop and the power loop separate. This facilitates a very clean design and greatly reduces or eliminates cross coupling. The PCB design can be optimised to take advantage of this feature.

4. Two-chip, integrated, normally-off power switch

The full graphic symbol of a GaN FET is shown in the pinning information section of the data sheet. Note that the symbol includes two devices:

- Low-voltage Si MOSFET with a p-n body diode
- High-voltage GaN FET without a p-n body diode

The full graphic symbol shows that the device is a two chip integrated switch. Functionally the switch is normally off. Internally the device is built with two chips. The high-voltage GaN HEMT or FET is normally on, which is the type most naturally made with GaN, and is combined with a high performance normally-off Si MOSFET specifically developed to complement the GaN HEMT. The two chips are integrated with absolute minimum inductance between them.

In circuit schematics where just the basic switching function is important, a simple N-channel FET symbol is used to represent the complete, integrated switch (see Q1 circled in red above). When you see the simple symbol, understand that it represents this two-chip integrated combination.
5. GaN FET limiting values

The limiting values table provides the range of operating conditions allowed for the GaN FET. The conditions are defined in accordance with the Absolute Maximum Rating System (IEC 60134).

Operation outside of these conditions is not guaranteed, so it is recommended that these values are never exceeded. Doing so risks immediate device failure or reduced lifetime of the GaN FET. To calculate how the limiting values change with temperature de-rating curves are provided.

The limiting values table for the GAN063-650WSA is given as an example of a standard limiting values table, in Table 2.

Table 2. Limiting values
In accordance with the Absolute Maximum Rating System (IEC 60134).

<table>
<thead>
<tr>
<th>Symbol</th>
<th>Parameter</th>
<th>Conditions</th>
<th>Min</th>
<th>Max</th>
<th>Unit</th>
</tr>
</thead>
<tbody>
<tr>
<td>( V_{DS} )</td>
<td>drain-source voltage</td>
<td>-55 °C ≤ ( T_j ) ≤ 175 °C</td>
<td>-</td>
<td>650</td>
<td>V</td>
</tr>
<tr>
<td>( V_{TDS} )</td>
<td>transient drain to source voltage</td>
<td>pulsed; ( t_p = 1 \mu s; \delta_{factor} = 0.01 )</td>
<td>-</td>
<td>800</td>
<td>V</td>
</tr>
<tr>
<td>( V_{GS} )</td>
<td>gate-source voltage</td>
<td>-20</td>
<td>20</td>
<td>V</td>
<td></td>
</tr>
<tr>
<td>( P_{tot} )</td>
<td>total power dissipation</td>
<td>( T_{mb} = 25 \degree C ); Fig. 8</td>
<td>-</td>
<td>143</td>
<td>W</td>
</tr>
<tr>
<td>( I_D )</td>
<td>drain current</td>
<td>( V_{GS} = 10 \ V; \ T_{mb} = 25 \degree C )</td>
<td>-</td>
<td>34.5</td>
<td>A</td>
</tr>
<tr>
<td>( I_{DM} )</td>
<td>peak drain current</td>
<td>( V_{GS} = 10 \ V; \ T_{mb} = 100 \degree C )</td>
<td>-</td>
<td>24.4</td>
<td>A</td>
</tr>
<tr>
<td>( T_{stg} )</td>
<td>storage temperature</td>
<td>-55</td>
<td>150</td>
<td>°C</td>
<td></td>
</tr>
<tr>
<td>( T_j )</td>
<td>junction temperature</td>
<td>-55</td>
<td>175</td>
<td>°C</td>
<td></td>
</tr>
<tr>
<td>( T_{sld(M)} )</td>
<td>peak soldering temperature</td>
<td>-</td>
<td>260</td>
<td>°C</td>
<td></td>
</tr>
</tbody>
</table>

Source-drain diode

<table>
<thead>
<tr>
<th>Symbol</th>
<th>Parameter</th>
<th>Conditions</th>
<th>Min</th>
<th>Max</th>
<th>Unit</th>
</tr>
</thead>
<tbody>
<tr>
<td>( I_S )</td>
<td>source current</td>
<td>( T_{mb} = 25 \degree C; \ V_{GS} = 0 \ V )</td>
<td>-</td>
<td>34.5</td>
<td>A</td>
</tr>
<tr>
<td>( I_{SM} )</td>
<td>peak source current</td>
<td>pulsed; ( t_p \leq 10 \mu s; \ T_{mb} = 25 \degree C )</td>
<td>-</td>
<td>150</td>
<td>A</td>
</tr>
</tbody>
</table>

5.1. Drain-source voltage, \( V_{DS} \)

This 650 V rating is the maximum value that will give you the desired product life.

GaN FETs do not have an avalanche breakdown mechanism. The Nexperia GaN FET does not typically show any significant leakage current until a \( V_{DS} \) well beyond 800 V is reached. So there is an extra margin in \( V_{DS} \) before excess leakage occurs. If the GaN FET is subjected to a sufficiently high voltage, well beyond the specified maximum, then because there is no clamping mechanism damage and failure will occur. Since GaN FETs do not have an avalanche breakdown mechanism they are immune to cosmic radiation and so no further derating is required.

- \( V_{DS} \) is the maximum voltage the device is guaranteed to block between drain and source terminals in the off-state. \( V_{DS} \) is a DC rating
- \( V_{DS} \) is not limited by avalanche breakdown; the rating can be applied over the entire operating range of -55 °C to 175 °C in contrast to the \( V_{DS} \) for a Si MOSFET which must be de-rated below 25 °C
5.2. Transient drain-source voltage, $V_{TDS}$

$V_{TDS}$ is the **Maximum** repetitive transient voltage the device is guaranteed to block between drain and source in the off state. This transient rating, applies over the entire operating temperature range.

### Table 4. Limiting values

<table>
<thead>
<tr>
<th>Symbol</th>
<th>Parameter</th>
<th>Conditions</th>
<th>Min</th>
<th>Max</th>
<th>Unit</th>
</tr>
</thead>
<tbody>
<tr>
<td>$V_{DS}$</td>
<td>drain-source voltage</td>
<td>$-55 \degree C \leq T_j \leq 175 \degree C$</td>
<td>-</td>
<td>650</td>
<td>V</td>
</tr>
<tr>
<td>$V_{TDS}$</td>
<td>transient drain to source voltage</td>
<td>pulsed; $t_p = 1 \mu s$; $\delta_{factor} = 0.01$</td>
<td>-</td>
<td>800</td>
<td>V</td>
</tr>
</tbody>
</table>

**Fig. 5. Duty Cycle Definition**

**Fig. 6. $V_{TDS}$ test circuit**

**Fig. 7. $V_{TDS}$ waveform**
5.3. Gate source voltage, $V_{GS}$ and total power dissipation, $P_{tot}$

$V_{GS}$

Maximum voltage the device is guaranteed to block between the gate and source terminals. This is a DC rating, and applies over the entire operating temperature range.

$P_{tot}$

$P_{tot}$ is the Total Power dissipation is the maximum for a device with a mounting base temperature of 25 °C.

$$P_{der} = \frac{P_{tot}}{P_{tot(25 \degree C)}} \times 100 \%$$

### Fig. 8. Normalised total power dissipation as a function of mounting base temperature

Power dissipation is calculated as that which would take the device to the maximum allowed junction temperature while keeping the mounting base at 25 °C.
5.4. Continuous and pulsed currents, $I_D$, $I_{DM}$, $I_S$ and $I_{SM}$.

<table>
<thead>
<tr>
<th>Symbol</th>
<th>Parameter</th>
<th>Conditions</th>
<th>Min</th>
<th>Max</th>
<th>Unit</th>
</tr>
</thead>
<tbody>
<tr>
<td>$V_{DS}$</td>
<td>drain-source voltage</td>
<td>$-55 \degree C \leq T_j \leq 175 \degree C$</td>
<td>-</td>
<td>650</td>
<td>V</td>
</tr>
<tr>
<td>$V_{TDS}$</td>
<td>transient drain to source voltage</td>
<td>pulsed; $t_p = 1 \mu s$; $\delta_{factor} = 0.01$</td>
<td>-</td>
<td>800</td>
<td>V</td>
</tr>
<tr>
<td>$V_{GS}$</td>
<td>gate-source voltage</td>
<td>-20</td>
<td>20</td>
<td>V</td>
<td></td>
</tr>
<tr>
<td>$P_{tot}$</td>
<td>total power dissipation</td>
<td>$T_{mb} = 25 \degree C$</td>
<td>-</td>
<td>143</td>
<td>W</td>
</tr>
<tr>
<td>$I_D$</td>
<td>drain current</td>
<td>$V_{GS} = 10 \text{ V}; T_{mb} = 25 \degree C$</td>
<td>-</td>
<td>34.5</td>
<td>A</td>
</tr>
<tr>
<td>$I_{DM}$</td>
<td>peak drain current</td>
<td>pulsed; $t_p \leq 10 \mu s$; $T_{mb} = 25 \degree C$</td>
<td>-</td>
<td>150</td>
<td>A</td>
</tr>
<tr>
<td>$T_{Sstg}$</td>
<td>storage temperature</td>
<td>$-55$</td>
<td>175</td>
<td>°C</td>
<td></td>
</tr>
<tr>
<td>$T_J$</td>
<td>junction temperature</td>
<td>$-55$</td>
<td>175</td>
<td>°C</td>
<td></td>
</tr>
<tr>
<td>$T_{sld(M)}$</td>
<td>peak soldering temperature</td>
<td>-</td>
<td>260</td>
<td>°C</td>
<td></td>
</tr>
</tbody>
</table>

The 25 °C current ratings are the same for both current directions ($I_D$ and $I_S$).

The maximum current at any $T_{mb}$ is the current which increases $T_J$ to the maximum allowed temperature (175 °C).
6. GaN FET static characteristics

These are the device parameters that explain how the GaN FET behaves in its normal operating conditions.

6.1. Gate-source threshold voltage, $V_{GS(th)}$

<table>
<thead>
<tr>
<th>Symbol</th>
<th>Parameter</th>
<th>Conditions</th>
<th>Min</th>
<th>Typ</th>
<th>Max</th>
<th>Unit</th>
</tr>
</thead>
<tbody>
<tr>
<td>$V_{GS(th)}$</td>
<td>gate-source threshold voltage</td>
<td>$I_D = 1 , mA; , V_{DS} = V_{GS}; , T_j = 25 , ^\circ C$</td>
<td>3.5</td>
<td>3.9</td>
<td>4.4</td>
<td>V</td>
</tr>
<tr>
<td></td>
<td></td>
<td>$I_D = 1 , mA; , V_{DS} = V_{GS}; , T_j = 175 , ^\circ C$</td>
<td>2.3</td>
<td>-</td>
<td>-</td>
<td>V</td>
</tr>
<tr>
<td>$I_{DSS}$</td>
<td>drain leakage current</td>
<td>$V_{DS} = 650 , V; , V_{GS} = 0 , V; , T_j = 25 , ^\circ C$</td>
<td>-</td>
<td>2</td>
<td>25</td>
<td>$\mu$A</td>
</tr>
<tr>
<td></td>
<td></td>
<td>$V_{DS} = 650 , V; , V_{GS} = 0 , V; , T_j = 175 , ^\circ C$</td>
<td>-</td>
<td>25</td>
<td>-</td>
<td>$\mu$A</td>
</tr>
<tr>
<td>$I_{GSS}$</td>
<td>gate leakage current</td>
<td>$V_{GS} = -20 , V; , V_{DS} = 0 , V; , T_j = 25 , ^\circ C$</td>
<td>-</td>
<td>10</td>
<td>100</td>
<td>nA</td>
</tr>
<tr>
<td></td>
<td></td>
<td>$V_{GS} = 20 , V; , V_{DS} = 0 , V; , T_j = 25 , ^\circ C$</td>
<td>-</td>
<td>10</td>
<td>100</td>
<td>nA</td>
</tr>
</tbody>
</table>

Gate-source threshold voltage for the GaN FET device is the gate-source threshold voltage of the Si MOSFET. This gate threshold is 3.9 V typically, with a negative temperature coefficient.

$I_D = 1 \, mA; \, V_{GS} = V_{GS(th)}$

Fig. 9. GaN FET gate-source threshold voltage
6.2. Drain-source on-state resistance, $R_{DSon}$

<table>
<thead>
<tr>
<th>$R_{DSon}$</th>
<th>drain-source on-state resistance</th>
<th>$V_{GS} = 10,\text{V}$; $I_D = 25,\text{A}$; $T_j = 25,\text{°C}$</th>
<th>-</th>
<th>50</th>
<th>60</th>
<th>mΩ</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td></td>
<td>$V_{GS} = 10,\text{V}$; $I_D = 25,\text{A}$; $T_j = 175,\text{°C}$</td>
<td>-</td>
<td>120</td>
<td>-</td>
<td>mΩ</td>
</tr>
</tbody>
</table>

Fig. 10. Test circuit for dynamic $R_{DSon}$

Fig. 11. Dynamic $R_{DSon}$ waveform

$R_{DSon}$ is the drain-to-source on-state resistance of the GaN FET. This has a dynamic value for GaN FETs. When $R_{DSon}$ is measured immediately after turn-on, following period of blocking high-voltage, this value will be slightly higher than normal. This is due to temporary charge trapping in the device structure. Nexperia have optimised the device so that charge trapping and dynamic $R_{DSon}$ are minimised.

As can be seen in Fig. 12, $R_{DSon}$ is shown as a normalised function of junction temperature.

![Figure 12](aaa-027810)

$$a = \frac{R_{DSon}}{R_{DSon(25\,\text{°C})}}$$

Fig. 12. Normalised drain-source on-state resistance as a function of junction temperature.
7. GaN FET dynamic characteristics

These are the device parameters that explain how the GaN FET behaves in its normal operating conditions.

7.1. Gate charge $Q_{G(tot)}$, $Q_{GS}$ and $Q_{GD}$

Gate charge for GaN FET is defined in the same way as a normal MOSFET, because the cascode arrangement of a GaN FET means that the gate is in fact the gate of a LV MOSFET. Since the LV MOSFET is a relatively small device it has a small gate charge suited to high speed switching.

7.2. Capacitances $C_{iss}$, $C_{oss}$ and $C_{rss}$

Traditional small signal capacitance is shown in Fig. 13. The discontinuity (step change) in Fig. 13 is where GaN HEMT pinches off. Capacitance relates charge to voltage and energy to voltage. For a linear capacitance, the following fundamental equations apply:

$$Q = CV$$

$$E = \frac{CV^2}{2}$$

![Fig. 13. Input, output and reverse transfer capacitance as a function of drain-source voltage; typical values](image)
The capacitances \( C_{o(er)} \) and \( C_{o(tr)} \) attempt to capture these relationships for a nonlinear capacitance.

### 7.3. Effective output capacitance (energy related), \( C_{o(er)} \)

The GaN FET capacitance parameter \( C_{o(er)} \) is the effective output capacitance (energy-related) dependent on the drain voltage.

Note that \( 0 \leq V_{DS} \leq 400 \text{ V} \) shown above, means as the voltage rises from 0 V to 400 V.

\[
E_{OSS} = \frac{Q_{OSS}}{V_{DS}} \cdot \frac{d}{dV_{DS}} \Rightarrow \int_{0}^{V_{DS}} C_{DS} \left( V_{DS} \right) \cdot dV_{DS}
\]

\[
E_{OSS} = \int_{0}^{V_{DS}} V_{DS} \cdot d\left( \frac{Q_{OSS}}{V_{DS}} \right) = \int_{0}^{V_{DS}} V_{DS} \cdot C_{DS} \left( V_{DS} \right) \cdot dV_{DS}
\]

**Fig. 14.** \( E_{OSS} \) as a function of \( V_{DS} \)

At a specific \( V_{DS} \), a unique value of \( C_{OSS} \) satisfies the equation:

\[
E_{OSS} = \frac{1}{2} \cdot C_{o(er)} \cdot V_{DS}^2
\]

e.g.

\[
E_{OSS} = \frac{1}{2} \cdot 190 \text{ pF} \cdot 400^2 = 15.2 \mu\text{J}
\]

By integrating \( C_{OSS} \) with respect to \( V_{DS} \), the result will be \( Q_{OSS} \). If we then integrate \( Q_{OSS} \) with respect to \( V_{DS} \), we will then arrive at \( E_{OSS} \).

\( E_{OSS} \) * switching frequency will give the switching power loss in Watts.
7.4. Effective output capacitance (time related), \( C_{o(tr)} \)

<table>
<thead>
<tr>
<th>( C_{o(er)} )</th>
<th>effective output capacitance, energy related</th>
<th>( 0 \leq V_{DS} \leq 400 \text{ V}; V_{GS} = 0 \text{ V}; T_j = 25 \text{ °C} )</th>
<th>-</th>
<th>190</th>
<th>-</th>
<th>pF</th>
</tr>
</thead>
<tbody>
<tr>
<td>( C_{o(tr)} )</td>
<td>effective output capacitance, time related</td>
<td>( 0 \leq V_{DS} \leq 400 \text{ V}; V_{GS} = 0 \text{ V}; T_j = 25 \text{ °C} )</td>
<td>-</td>
<td>310</td>
<td>-</td>
<td>pF</td>
</tr>
</tbody>
</table>

The GaN FET capacitance parameter \( C_{o(tr)} \) is the equivalent capacitance to give same charging time, as \( V_{DS} \) rises from 0 V to 400 V. This can also be described as a constant current being used to charge the output capacitance, giving a time related effective value.

\[
Q_{oss} = \int_0^V dq = \int_0^V C \left( V_{DS} \right) dV_{DS}
\]

At a specific \( V_{DS} \), a unique value of \( C_{oss} \) satisfies the equation:

\[
V_{ds} = \frac{Q_{oss}}{C_{o(tr)}} = \frac{1}{C_{o(tr)}} \int_0^t i(t) \cdot dt
\]

e.g.

\[
400V = \frac{1}{310 \text{ pF}} \cdot \int_0^{120\text{ns}} 1.0A \cdot dt
\]

\[
Q_{oss} = 124nC
\]
7.5. Output charge and stored energy, $Q_{\text{OSS}}$ and $E_{\text{OSS}}$

Rather than using the $C_{\text{O(tr)}}$ and $C_{\text{O(er)}}$ parameters, it is much easier to use the graphs shown below that are also available in the data sheet. The respective $Q_{\text{OSS}}$ and $E_{\text{OSS}}$ values can be read directly for the required $V_{DS}$.

![Graph of $Q_{\text{OSS}}$ vs $V_{DS}$](image1)

![Graph of $E_{\text{OSS}}$ vs $V_{DS}$](image2)

Fig. 15. Typical $Q_{\text{OSS}}$

Fig. 16. Typical $E_{\text{OSS}}$ stored energy

7.6. GaN FET switching time characteristics

Nexperia GaN FETs generally require a ferrite bead in series with the gate. This serves to de-Q the gate-source loop and improve the switching stability. The ferrite bead effectively provides damping impedance at frequencies > 100 MHz. It also introduces a small propagation delay, however it does not introduce any additional loss.

The GAN063-650WSA in TO247 package has an integral ferrite bead, and so an external bead is not required. Newer GaN FETs may not include the integral ferrite bead, and so one must be included in the external gate drive. *Always refer to the data sheet of specific devices for details.*

![Diagram of switching time waveform](image3)

Fig. 17. Switching time waveform

![Diagram of internal ferrite bead](image4)

Fig. 18. Internal Ferrite bead
7.7. Source-drain voltage, \( V_{SD} \)

This device parameter source-drain voltage refers to the GaN FET device when it is acting as a two terminal device when not enhanced with the gate \( V_{GS} = 0 \) V.

<table>
<thead>
<tr>
<th>Source-drain voltage</th>
<th>( I_S = 25 ) A; ( V_{GS} = 0 ) V; ( T_j = 25 ) °C</th>
<th>-</th>
<th>1.9</th>
<th>-</th>
<th>V</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>( I_S = 12.5 ) A; ( V_{GS} = 0 ) V; ( T_j = 25 ) °C</td>
<td>-</td>
<td>1.35</td>
<td>-</td>
<td>V</td>
</tr>
<tr>
<td>( t_r ) reverse recovery time</td>
<td>( I_S = 25 ) A; ( \frac{dI_S}{dt} = -1000 ) A/( \mu )s; ( V_{GS} = 0 ) V; ( V_{DS} = 400 ) V</td>
<td>-</td>
<td>54</td>
<td>-</td>
<td>ns</td>
</tr>
<tr>
<td>( Q_r ) recovered charge</td>
<td>-</td>
<td>125</td>
<td>-</td>
<td>nC</td>
<td></td>
</tr>
</tbody>
</table>

Fig. 19. Source-drain (diode forward) current as a function of source-drain (diode forward) voltage; typical values

Fig. 20. Source-drain (diode forward) voltage

\( V_{SD} \) is the voltage developed whilst GaN FET conducts in reverse direction (e.g. acting as a rectifier carrying freewheeling current) Here the voltage \( V_{SD} \) comprises the forward voltage of the Silicon MOSFET body diode and the voltage drop across the 2 DEG channel of the GaN HEMT.
8. \( Q_r \) for GaN FET switches

The Device Under Test (DUT) is carrying a freewheeling current. The switch in the high side of the test circuit in Fig. 21 will then turn on and force a transition at the switching node from low voltage to high voltage. This will cause the current in the DUT to change from freewheeling current to some negative current up until the point that the DUT is blocking the full DC supply voltage. If you integrate the negative current you will get the minority carrier stored change plus any output capacitance charge.

For GaN FETs, the charge on the output capacitance \( Q_{OSS} \) is the dominant component of the reverse recovery charge \( Q_r \). Hence the reason that the datasheet for the Nexperia GaN FET specifies the same value for both \( Q_{OSS} \) and \( Q_r \).

Some GaN device manufacturers will claim to have zero reverse recovery charge \( Q_r \) because they do not have a PN junction body diode. However, they will still have \( Q_{OSS} \).
9. Switching-node snubber

To achieve maximum efficiency and stability when switching high currents, a switching node RC snubber \((R_{SN}, C_{SN})\) is recommended. For \(I_L < 14\) A, a switching-node snubber is not required.

Note: a DC-link snubber is recommended in all cases. Optimal is 20 nF in series with 4 \(\Omega\), most easily achieved with parallel combination 10 nF and 8 \(\Omega\). This snubber lowers the Q factor of any resonance in the bus. That resonance will act as a load on the high gain amplifier that is the GaN FET and can lead to instability.

For some GaN FETs, like the GAN063-650WSA, an RC snubber is recommended for the switching node. This will increase switching loss, so this is only recommended at high power levels where the losses are a very small percentage of the total power. Other GaN FETs do not require a snubber on the switching node at any power level. **Always refer to the data sheet of specific devices for details.**

10. Revision history

<table>
<thead>
<tr>
<th>Revision number</th>
<th>Date</th>
<th>Description</th>
</tr>
</thead>
<tbody>
<tr>
<td>2.0</td>
<td>2020-06-08</td>
<td><strong>Section 5.1, Section 7.6 and Section 9</strong> updated</td>
</tr>
<tr>
<td>1.1</td>
<td>2019-02-13</td>
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